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THE GRAVITATIONAL FIELD OF A ROTATING INFINITE CYLINDRICAL SHELL

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A B S T R A C T.

Israel's method for treating surface layers is applied to determine the gravitational field due to a rotating cylindrical shell. The interior space-time is flat while the exterior metric can be one of three types. For a given value of the stress in the cylinder, the type of the exterior metric depends on the mass per unit co-ordinate length of the cylinder.

1. INTRODUCTION

The problem of determining the gravitational field due to a rotating infinite cylindrical shell has been discussed by Frehland (1972) and Papapetrou, Macedo and Som (1978). However in these papers the authors have restricted their attention to one form of the exterior metric whereas it is known (Van Stockum 1937, Tipler 1974, Bonnor 1980) that there are three real forms for the exterior metric depending on whether a certain constant of integration is positive, negative or zero. In the present work we shall use Israel's (1966) method for constructing shell sources to match in their most general form, the three exterior forms of the metric to the interior metric, which is necessarily flat (Davies and Caplan, 1971). It is shown that the form of the exterior metric depends on whether the mass per unit coordinate length of the cylinder is less than, equal to or greater than a certain critical value. As a particular example we discuss briefly the case of a shell composed of dust.

In Section 2 we calculate the three exterior and the interior vacuum metrics for a stationary cylindrically symmetric field in their most general form. In Section 3 we apply these metrics to the problem of an infinite cylindrical shell of coordinate radius  $r = a$  and find the surface energy tensor and mass per unit coordinate length of the shell for each of the three exterior metrics. In Section 4 we give the restrictions on the metric constants, imposed by physical considerations. In Section 5 we evaluate the proper density and the principal stresses on the shell, which we then use in Section 6 to show that for a given

stress, the value of the mass per unit coordinate length determines the type of exterior metric.

§2. GENERAL SOLUTION FOR A STATIONARY CYLINDRICALLY SYMMETRIC VACUUM FIELD.

A stationary field with cylindrical symmetry has a metric of the form

$$(ds)^2 = - e^{2\lambda} (dt + v d\phi)^2 + e^{-2\lambda} [e^{2\gamma} (dr^2 + dz^2) + r^2 d\phi^2] , \quad (2.1)$$

where  $r, z, \phi$  are cylindrical coordinates and  $\lambda, v$  and  $\gamma$  are functions of  $r$  only. The vacuum field equations  $R_{ij} = 0$  reduce to

$$\frac{d^2 \lambda}{dr^2} + \frac{1}{r} \frac{d\lambda}{dr} + \frac{1}{2r^2} e^{4\lambda} \left(\frac{dv}{dr}\right)^2 = 0 , \quad (2.2)$$

$$\frac{d^2 v}{dr^2} - \frac{1}{r} \frac{dv}{dr} + 4 \frac{d\lambda}{dr} \cdot \frac{dv}{dr} = 0 \quad (2.3)$$

and

$$\frac{d\gamma}{dr} - r \left(\frac{d\lambda}{dr}\right)^2 + \frac{1}{4r} e^{4\lambda} \left(\frac{dv}{dr}\right)^2 = 0 . \quad (2.4)$$

The first integral of (2.3) is

$$\frac{dy}{dr} = 2br e^{-4\lambda}, \quad (2.5)$$

where  $b$  is a constant and substituting this into (2.2) yields

$$\frac{d^2\lambda}{d\rho_1^2} + \frac{1}{\rho_1} \frac{d\lambda}{d\rho_1} + 2e^{-4\lambda} = 0, \quad (2.6)$$

where  $\rho_1 = br$ . The transformation  $\rho_1 = e^x$ ,  $y = \lambda - \frac{1}{2}x$  then gives

$$\frac{d^2y}{dx^2} = -2e^{-4y}, \quad (2.7)$$

which has a first integral of the form

$$dx = \pm \frac{dy}{\sqrt{e^{-4y} + P}}$$

where  $P$  is a constant.

We distinguish three different types of solution as follows :

Case (i) where  $P > 0$ , Case (ii) where  $P < 0$  and Case (iii) where  $P = 0$ .

In each of the three cases equation (2.8) is easily integrated and on substituting the subsequent expression for  $\lambda$  in equations (2.4) and (2.5) we eventually obtain the following three forms for the metric :

$$\text{Case (i)} \quad (ds)^2 = -\frac{1}{\alpha_1^2} [\rho^{1-c} - \rho^{1+c}] dt^2$$

$$\begin{aligned} & + \frac{2}{\alpha_2^2} \left[ \left( \frac{\alpha-2G}{2\omega} \right)^{1+c} \rho^{1+c} + \left( \frac{\alpha+2G}{2\omega} \right)^{1-c} \rho^{1-c} \right] d\phi dt \\ & + \frac{1}{\alpha_1^2} \left[ \left( \frac{\alpha-2G}{2\omega} \right)^{2(1+c)} \rho^{2(1+c)} - \left( \frac{\alpha+2G}{2\omega} \right)^{2(1-c)} \rho^{2(1-c)} \right] d\phi \\ & + D \rho^{\frac{1}{2}(c-1)} (dr^2 + dz^2) \end{aligned} \quad (2.9)$$

where  $\alpha_1^2 = \alpha_2^2 = \alpha^2$ ,  $\rho = |\omega|r$  and  $\alpha, c, D, G$  and  $\omega$  are constants;

$$\begin{aligned} \text{Case (ii)}, \quad (ds)^2 = & -\frac{2\omega r}{\alpha_1^2} \sin\beta dt^2 + \frac{2rc}{\alpha_2^2} [\cos\beta - \frac{2G}{\alpha} \sin\beta] d\phi dt \\ & + \frac{2rc}{\omega\alpha_1^2} \left[ \left( \frac{\alpha}{2} - \frac{G^2}{\alpha} \right) \sin\beta + G \cos\beta \right] d\phi^2 \\ & + D \rho^{-\frac{1}{2}(1+c)} (dr^2 + dz^2) \end{aligned} \quad (2.10)$$

where  $\rho = |\omega|r$ ,  $\beta = c \log \rho$  and  $\alpha, c, D, G$  and  $\omega$  are constants and again  $\alpha_1^2 = \alpha_2^2 = \alpha^2$ ;

$$\begin{aligned} \text{Case (iii)}, \quad (ds)^2 = & -2br \log \rho dt^2 + 2\epsilon r (1-2G \log \rho) d\phi dt \\ & + \frac{2Gr}{b} [1 - G \log \rho] d\phi^2 + D \rho^{-\frac{1}{2}} (dr^2 + dz^2) \end{aligned} \quad (2.11)$$

where  $\rho = |\omega|r$ ,  $\epsilon = \pm 1$  and  $b, D, G$  and  $\omega$  are constants.

The above three cases correspond to the three types of cylindrically symmetric metric discussed by Van Stockum (1937), Tipler (1974) and Bonnor (1980). In constructing a cylindrical shell source, Frehland (1972) and Papapetron et al. (1978) consider only Case (i). In the following sections all three cases will be studied.

We notice that, by means of the complex transformation  $c \rightarrow ic$ ,  $\alpha \rightarrow i\alpha$ ,  $\alpha_1 \rightarrow i\alpha_1$ ,  $\alpha_2 \rightarrow i\alpha_2$ , we can obtain the Case (ii) metric from Case (i), as has been mentioned by Kramer, Stephani, MacCallum and Herlt (1980).

Case (i) is Petrov type I for all non-zero values of  $c$ , except  $c = \pm 1$  when it is flat and  $c = \pm 3$  when it is Petrov type D. Case (ii) is Petrov type I for all non-zero values of  $c$  and Case (iii) is Petrov type II.

The three cases above give the complete general solution for a stationary vacuum field exterior to a cylindrically symmetric source. For the interior vacuum solution we can simplify these considerably using the requirements that the curvature invariants be non-singular along the axis  $r = 0$  and that elementary flatness holds along this axis.

In Case (iii) both the metric and its curvature invariants are singular at  $r = 0$ .

In Case (ii) the curvature invariants are non-singular at  $r = 0$  only if  $c^2 \geq 3$ , but the metric does not satisfy elementary flatness there.



In Case (i) both the metric and its invariants are non-singular on the axis  $r = 0$  only if  $c^2 = 1$ , in which case the metric is Minkowskian. Applying the elementary flatness condition at  $r = 0$  we obtain the metric

$$(ds)^2 = -\frac{1}{D} dt^2 + Dr^2 \left(\frac{\omega}{D} dt + d\phi\right)^2 + D(dr^2 + dz^2). \quad (2.12)$$

Without loss of generality we can take  $\omega = 0$  in (2.12) since the transformation

$$\phi' = \frac{\omega}{D} t + \phi$$

will reduce (2.12) to the form

$$(ds)^2 = -\frac{1}{D} dt^2 + Dr^2 d\phi^2 + D(dr^2 + dz^2), \quad (2.13)$$

which is the most general interior vacuum cylindrically symmetric metric. This is the interior metric used by Papapetron et al. (1978).

To avoid confusion with the constants in the exterior metric we will use the interior metric

$$(ds)^2 = -\frac{1}{L_0} dt^2 + L_0 r^2 d\phi^2 + L_0 (dr^2 + dz^2). \quad (2.14)$$

53: INFINITE CYLINDRICAL SHELL.

We apply Israel's (1966) method for surface layers to the interior metric (2.14) and the three exterior metrics of the previous section and thus construct, in its most general form, the gravitational field of an infinite shell. We assume that the coordinates  $(t, r, z, \phi)$  are the same both inside and outside of the shell.

Case (1) :

Let the history,  $\Sigma$ , of the shell be given by  $r = a$ .

The metric on  $\Sigma$  induced by its embedding in the interior space-time is

$$ds_{-}^2 = -\frac{1}{L_0} dt^2 + L_0 a^2 d\phi^2 + L_0 dz^2 \quad (3.1)$$

and that due to its embedding in the exterior space-time is

$$\begin{aligned} ds_{+}^2 = & -\frac{1}{\alpha_1} (\rho_0^{1-c} - \rho_0^{1+c}) dt^2 \\ & + \frac{2}{\alpha_2} \left[ \left( \frac{\alpha-2G}{2w} \right) \rho_0^{1+c} + \left( \frac{\alpha+2G}{2w} \right) \rho_0^{1-c} \right] d\phi dt \\ & + \frac{1}{\alpha_1} \left[ \left( \frac{\alpha-2G}{2w} \right)^2 \rho_0^{1+c} - \left( \frac{\alpha+2G}{2w} \right)^2 \rho_0^{1-c} \right] d\phi^2 \\ & + D \rho_0^{\frac{1}{2}} (c^2 - 1) dz^2, \end{aligned} \quad (3.2)$$

where  $\rho_0 = |w| a$ . The condition

$$ds_{-}^2 = ds_{+}^2 \quad (3.3)$$

yields three independent equations for the six unknowns

$L_0$ ,  $\alpha$ ,  $c$ ,  $D$ ,  $G$  and  $\omega$ . These are

$$L_0 = D \rho_0^{\frac{1}{2}(c^2-1)}, \quad (3.4)$$

$$\rho_0^{1-c} = \frac{\alpha_1(\alpha-2G)}{2\alpha L_0} \quad (3.5)$$

$$\text{and } \rho_0^{1+c} = -\frac{\alpha_1(\alpha+2G)}{2\alpha L_0}. \quad (3.6)$$

In general, if  $x_+^i$  ( $i = 0, 1, 2, 3$ ) are the exterior coordinates and  $x_+^i = x_+^i(\xi^\mu)$  ( $\mu = 0, 2, 3$ ) is the equation of the shell regarded as embedded in the exterior space-time, then the second fundamental form of  $\Sigma$  due to this embedding is

$$K_{\mu\nu}^+ = n^+_{i/j} \frac{\partial x_+^i}{\partial \xi^\mu} \frac{\partial x_+^j}{\partial \xi^\nu} \quad (3.7)$$

where the vertical stroke indicates covariant derivative with respect to the exterior metric and  $n^+_{i/j}$  is a unit vector normal to  $\Sigma$ . In the same way the interior second fundamental form is

$$K_{\mu\nu}^- = n^-_{i/j} \frac{\partial x_-^i}{\partial \xi^\mu} \frac{\partial x_-^j}{\partial \xi^\nu} \quad (3.8)$$

where the minus signs refer in an obvious way to the interior space-time. Defining  $\gamma_{\mu\nu}$  by

$$\gamma_{\mu\nu} = K_{\mu\nu}^+ - K_{\mu\nu}^- \quad (3.9)$$

the surface energy tensor,  $S_{\mu\nu}$ , of the shell is given by

$$-\kappa S_{\mu\nu} = \gamma_{\mu\nu} - g_{\mu\nu} \gamma, \quad (3.10)$$

where  $g_{\mu\nu}$  is the intrinsic metric on  $\Sigma$ ,  $\gamma = \gamma^\mu{}_\mu$  and  $\kappa = 8\pi$ . The calculation of  $S_{\mu\nu}$  is considerably simplified here since we are taking

$$(x_+^0, x_+^1, x_+^2, x_+^3) \equiv (x_-^0, x_-^1, x_-^2, x_-^3) \equiv (t, r, z, \phi) \quad (3.11)$$

and hence the intrinsic coordinates on  $\Sigma$  are

$$(\xi^0, \xi^2, \xi^3) = (t, z, \phi). \quad (3.12)$$

After some manipulation using (3.4), (3.5) and (3.6) we find that the non-zero components of the surface energy tensor are

$$S_{00} = \frac{1}{4\kappa a L_0^{3/2}} \left[ 3 + \frac{4Gc}{\alpha} - c^2 \right], \quad (3.13)$$

$$S_{30} = S_{03} = -\frac{\alpha_1 c L_0^{1/2} a \omega}{\alpha_2 \alpha \kappa} = \pm \frac{a \omega c L_0}{\alpha \kappa} \quad (3.14)$$

$$\text{and } S_{33} = \frac{a L_0^{1/2}}{4\kappa} \left[ 1 + \frac{4Gc}{\alpha} + c^2 \right]. \quad (3.15)$$

Adapting Whittaker's (1935) theorem to the case of a surface layer (see McCrea 1976) we define the total mass,  $M$ , of the shell to be

$$M = \int_{\Sigma} (-S^0{}_0 + S^2{}_2 + S^3{}_3) \sqrt{-g^{(3)}} dz d\phi \quad (3.16)$$

Clearly the mass will be infinite, but we can calculate the mass per unit length of  $z$ ,  $M_1$ , to be

$$M_1 = \frac{dM}{dz} = \frac{1}{4} \left( 1 + \frac{2Gc}{\alpha} \right). \quad (3.17)$$

This agrees with the results of Papapetrou et. al. (1978).

Case (ii):

In this case we take (2.14) as the interior and (2.10) as the exterior metric. Condition (3.3) yields the following three independent equations for the six unknowns  $L_0$ ,  $\alpha$ ,  $c$ ,  $D$ ,  $G$  and  $\omega$ :

$$\sin \beta_0 = \frac{\alpha_1}{2a\omega L_0}, \quad (3.18)$$

$$\cos \beta_0 = \frac{\alpha_1 G}{\alpha a \omega L_0}, \quad (3.19)$$

$$\text{and } D = \rho_0^{-\frac{1}{2}(1+c^2)}, \quad (3.20)$$

where  $\rho_0 = |\omega|a$  and  $\beta_0 = c \log \rho_0$ .

Continuing as in Case (i) we can calculate the surface energy tensor,  $S_{\mu\nu}$  and find the only non-zero components to be

$$S_{00} = \frac{1}{4\kappa a L_0^{3/2}} \left[ 3 + \frac{4Gc}{\alpha} + c^2 \right] \quad (3.21)$$

$$S_{03} = S_{30} = \frac{\alpha_1 c a \omega L_0^{\frac{1}{2}}}{\alpha_2 \alpha \kappa} = \pm \frac{c a \omega L_0^{\frac{1}{2}}}{\alpha \kappa}, \quad (3.22)$$

and 
$$S_{33} = \frac{aL_0}{4\kappa} \left[ 1 + \frac{4Gc}{\alpha} - c^2 \right], \tag{3.23}$$

where again  $\kappa = 8\pi$ . The mass per unit length of  $z$ , as defined in (3.16) and (3.17), for this case is

$$M_1 = \frac{1}{4} \left( 1 + \frac{2Gc}{\alpha} \right). \tag{3.24}$$

Case (iii):

Matching the interior metric (2.14) to the exterior metric (2.11), as in the previous cases, yields three independent equations for the five unknowns  $L_0$ ,  $b$ ,  $D$ ,  $G$  and  $\omega$ . These are

$$L_0 = D\rho_0^{-\frac{1}{2}} \tag{3.25}$$

$$2G \log \rho_0 = 1 \tag{3.26}$$

and 
$$G = abL_0, \tag{3.27}$$

where  $\rho_0 = |\omega|a$ . Using these, the non-zero components of the surface energy tensor  $S_{\mu\nu}$  can be shown to be

$$S_{00} = \frac{1}{4\kappa a L_0^{3/2}} [3 + 4G], \tag{3.28}$$

$$S_{03} = S_{30} = \frac{\epsilon abL_0^{\frac{1}{2}}}{\kappa} \tag{3.29}$$

$$\text{and } S_{33} = \frac{\alpha L_0^{\frac{1}{2}}}{4K} [1 + 4G]. \quad (3.30)$$

The mass per unit length of  $z$  reduces to

$$M_1 = \frac{1}{4} [1 + 2G]. \quad (3.31)$$

#### §4. RESTRICTIONS ON THE SURFACE ENERGY TENSOR.

Following Hawking and Ellis (1973) we require that for any vector  $u^i$  such that  $g_{ij} u^i u^j \leq 0$ , an energy tensor  $T_{ij}$ , must satisfy the following restrictions:

$$T_{ij} u^i u^j \geq 0, \quad (4.1)$$

$$T_{ij} u^j \text{ is non-spacelike}, \quad (4.2)$$

$$\text{and } T_{ij} u^i u^j \geq \frac{1}{2} T(u^i u_i), \text{ where } T = T^i_i. \quad (4.3)$$

Taking the non-zero components of the surface energy tensor,  $S_{\mu\nu}$  with respect to the orthonormal base

$$e^\mu_{(0)} = L_0^{\frac{1}{2}} \delta^\mu_0, \quad e^\mu_{(3)} = \frac{1}{aL_0^{\frac{1}{2}}} \delta^\mu_3, \quad (4.4)$$

the above restrictions take the form

$$S_{(00)} \geq 0, \quad (4.5)$$

$$S_{(00)} \geq |S_{(33)}|, \quad (4.6)$$

$$S_{(00)} + S_{(33)} \geq 2|S_{(03)}|$$

$$\text{and } S_{(00)} \geq |S_{(03)}|. \quad (4.8)$$

Applying these to the surface energy tensors in each of the three cases one obtains the following results :

Case (i)

$$c^2 \leq 1, \quad (4.9)$$

$$\text{and } 1 + \frac{4Gc}{\alpha} + c^2 \geq 0; \quad (4.10)$$



Case (ii)

$$1 + \frac{4Gc}{\alpha} - c^2 \geq 0 ; \quad (4.11)$$

Case (iii)

$$1 + 4G \geq 0 . \quad (4.12)$$

Clearly these restrictions ensure that the mass per unit coordinate length is positive for each of the three cases, as given by (3.17), (3.24) and (3.31) .

#### §5. THE SURFACE DENSITY AND PRINCIPAL STRESSES ON THE SHELL.

We calculate the eigenvalues of the surface energy tensor and hence obtain the proper surface density,  $\mu$ , and the principal stresses in the  $z$  and  $\phi$  - directions, written  $\sigma_z$  and  $\sigma_\phi$  respectively.

For convenience we use the orthonormal components  $S_{(\mu\nu)}$  of Section 4. Since  $S_{(2\mu)} = 0$ ,  $\sigma_z = 0$  in all three cases and so the eigenvector equation reduces to the simple  $2 \times 2$  tensor equation

$$S_{(AB)} u^B = \lambda \eta_{AB} u^B, \quad (5.1)$$

where  $A, B = 0, 3$  and  $\eta_{AB} = \text{diag. } (-1, 1)$ . Solving (5.1) yields two eigenvectors, one timelike and one spacelike with the corresponding eigenvalues  $\lambda_{(0)}$  and  $\lambda_{(3)}$  respectively. The proper surface density  $\mu = -\lambda_{(0)}$  and the principal stress in the  $\phi$ -direction  $\sigma_\phi = -\lambda_{(3)}$ . It is found that for all three cases

$$\mu = p(q + 2\sqrt{8M_1 - q}), \quad (5.2)$$

$$\sigma_\phi = p(q - 2\sqrt{8M_1 - q}), \quad (5.3)$$

$$\text{where } p = \frac{1}{4kaL_0^{\frac{1}{2}}}, \quad (5.4)$$

and

$$\text{for Case (i)} \quad q = 1 - c^2, \quad 1 \geq c^2 > 0, \quad (5.5)$$

$$\text{for Case (ii)} \quad q = 1 + c^2, \quad c^2 > 0, \quad (5.6)$$

$$\text{for Case (iii)} \quad q = 1. \quad (5.7)$$

$M_1$  is given by (3.17), (3.24) and (3.31) for Cases (i), (ii) and (iii) respectively.

A simple calculation in each of the three cases shows that the limitations on the constants contained in the previous section ensure that  $\mu$  is real and positive and that  $\sigma_\phi$  is real in each case, so the densities and stresses are physically reasonable.

§6. GENERAL DISCUSSION.

In Cases (i) and (ii) matching the interior and exterior metrics for a given radius yields three equations for six unknowns, so we require three further conditions to completely determine the metric. This is reasonable since the physical quantities such as mass and stress will affect the metric. If we fix the mass per unit length  $M_1$ , the density  $\mu$  and the stress  $\sigma_\phi$  we can determine all the constants and so both interior and exterior metrics are known.

In Case (iii) however we have only five unknowns and so for a given radius, if two of the physical quantities are fixed we can evaluate all the constants and hence the metric.

A further interesting point is that given  $\sigma_\phi/p$ , the value of the mass per unit length,  $M_1$ , determines whether the exterior metric is Case (i), (ii) or (iii). We can show this by writing  $M_1$  in terms of  $\sigma_\phi$  using (5.3), which results in the equation

$$M_1 = \frac{1}{32} [(q - z)^2 + 4q] , \quad (6.1)$$

where  $z = \frac{\sigma_\phi}{p}$ , and  $0 \leq q < 1$  in Case (i),  $q > 1$  in Case (ii) and  $q = 1$  in Case (iii). Since, by (5.3),  $z \leq q$  in all three cases, we obtain the following general classification:

For  $z \leq 0$  :

$$\text{In Case (i), } \frac{1}{32} z^2 \leq M_1 < \frac{1}{32} (z^2 - 2z + 5) \quad (6.2)$$

$$\text{in Case (ii), } M_1 > \frac{1}{32} (z^2 - 2z + 5) \quad (6.3)$$

$$\text{in Case (iii), } M_1 = \frac{1}{32} (z^2 - 2z + 5) \quad (6.4)$$

For  $0 < z < 1$  :

$$\text{In Case (i) } \frac{1}{8} z \leq M_1 < \frac{1}{32} (z^2 - 2z + 5) \quad (6.5)$$

$$\text{in Case (ii) } M_1 > \frac{1}{32} (z^2 - 2z + 5) \quad (6.6)$$

$$\text{in Case (iii) } M_1 = \frac{1}{32} (z^2 - 2z + 5) \quad (6.7)$$

For  $z = 1$  :

Case (i) is not possible since  $z \leq q < 1$  ,

$$\text{in Case (ii) } M_1 > \frac{1}{8} \quad (6.8)$$

$$\text{in Case (iii) } M_1 = \frac{1}{8} \quad (6.9)$$

For  $z > 1$  :

$$\text{Only Case (ii) can occur and } M_1 > \frac{1}{8} z . \quad (6.10)$$

We can see that provided  $z$  is fixed, then the value of  $M_1$  determines whether the exterior metric is Case (i), (ii) or (iii).

For the purpose of comparison, consider a cylindrical shell composed of dust, as discussed by Papapetrou et al. (1978). The stress  $\sigma_\phi$  will, by definition of a dust, be zero (this is equivalent to the condition in the above paper that  $T_{00} T_{33} = T_{03}^2$ ) and the inequalities (6.2), (6.3), (6.4) reduce to

$$0 \leq M_1 < \frac{5}{32} \quad \text{for Case (i) ,}$$

$$M_1 > \frac{5}{32} \quad \text{for Case (ii)}$$

$$\text{and } M_1 = \frac{5}{32} \quad \text{for Case (iii) .}$$

The extension of the solution to three exterior metrics completes the picture and allows a full range of values for the mass per unit length  $M_1$ , rather than the restricted range of Case (i) as studied by Papapetrou et al. (1978) .

We note finally that if  $u^a \equiv (u^0, 0, 0, u^3)$  are the orthonormal tetrad components of the timelike eigenvector (i.e. the four-velocity) then

$$(u^3/u^0)^2 = (4M_1 - \sqrt{8M_1 - q}) / (4M_1 + \sqrt{8M_1 - q}) \quad (6.11)$$

so that  $(u^3/u^0)^2 \rightarrow 1$  as  $q \rightarrow 8M_1$ . From (5.2) and (5.3) it follows that in all three cases the four-velocity becomes null as  $\sigma_\phi \rightarrow \mu$ .

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